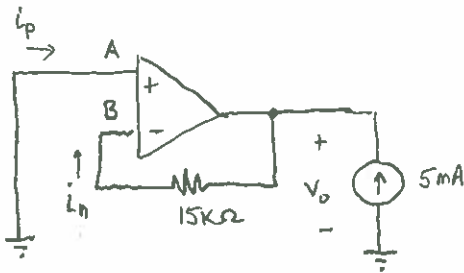


Problem 1

(a)



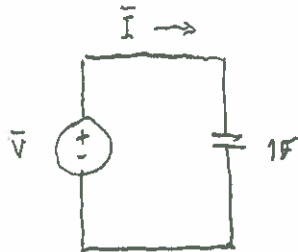
At node A, $V_A = 0$

And $V_B = 0$

At node B, $\frac{V_B - V_0}{15k} - i_n = 0$, so $V_0 = V_B$

Therefore, $V_0 = 0$

(b)



where $v(t) = \sin(t)$
 $= \cos(t - 90^\circ)$

and $\bar{V} = 1 \angle -90^\circ$

For the capacitor, $Z_c = \frac{1}{j\omega C}$ where $\omega = 1 \text{ rad/sec}$
 $C = 1 \text{ F}$

so $Z_c = -j \Omega$

Therefore, $\bar{I} = \frac{\bar{V}}{Z_c} = \frac{1 \angle -90^\circ}{-j} = \frac{1 \angle -90^\circ}{1 \angle -90^\circ}$

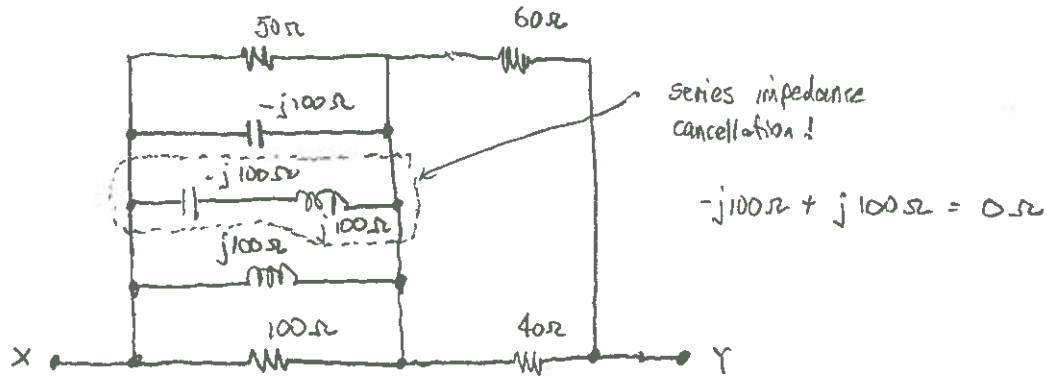
$\bar{I} = 1 \text{ A}$

(c) We have $\omega = 100 \text{ rad/sec}$, so the impedances of the inductors and capacitors will be

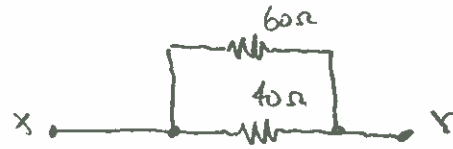
$$Z_L = j\omega L = j(100) \times 1 = +j100 \Omega$$

$$Z_C = \frac{1}{j\omega C} = \frac{1}{j(100)(100 \times 10^{-6})} = -j100 \Omega$$

The circuit is :

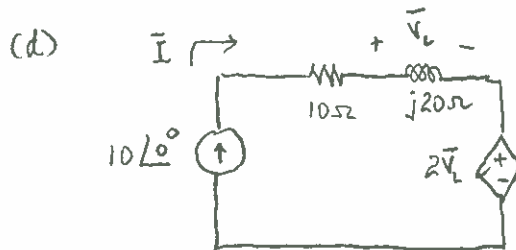


The circuit simplifies simply to



$$Z_{eq} = \frac{60 \times 40}{60 + 40}$$

$$Z_{eq} = 24\Omega$$



We know $V_L = I(j20)$

so $V_L = 10 \angle 0^\circ (j20)$

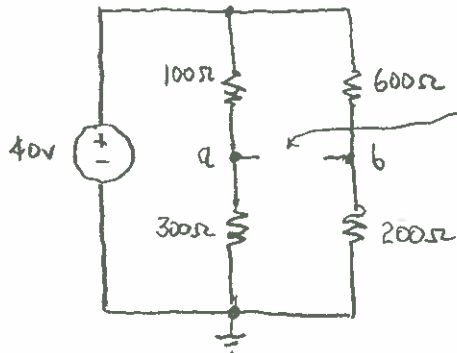
$$V_L = 200 \angle 90^\circ$$

Complex power $\bar{S} = \frac{1}{2} \bar{V} \bar{I}^*$, where $\bar{V} = 2V_L = 400 \angle 90^\circ$

$$\bar{S} = \frac{1}{2} (400 \angle 90^\circ) (10 \angle 0^\circ)$$

$$\bar{S} = 2000 \angle 90^\circ = j2000 \text{ VA}$$

(e)



Capacitor behaves as an open circuit at D.C.

We need the voltage V_{ab} to determine the energy.

We have two voltage dividers

$$V_a = \frac{300}{300 + 100} \times 40 = 30 \text{ v}$$

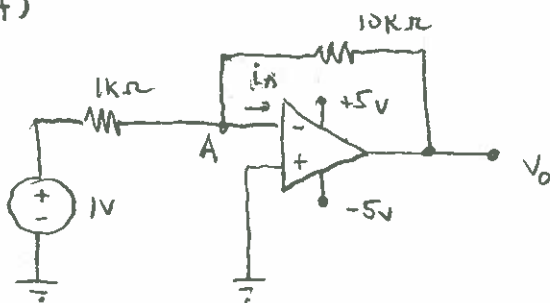
$$V_b = \frac{200}{200 + 600} \times 40 = 10 \text{ v}$$

$$\text{so } V_{ab} = 30 - 10 = 20 \text{ v.}$$

Energy in the capacitor: $w = \frac{1}{2} C v^2 = \frac{1}{2} (0.1) (20^2)$

$$w = 20 \text{ J}$$

(f)



At node A,

$$\frac{V_A - 1}{1\text{k}\Omega} + \frac{V_A - V_o}{10\text{k}\Omega} - i_n = 0$$

$$\text{and } V_A = 0$$

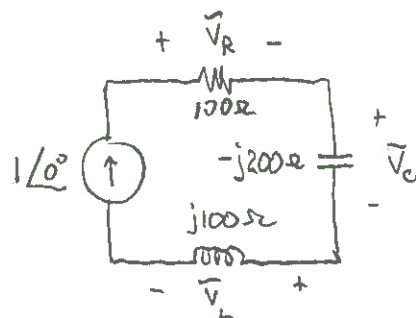
$$\frac{0 - 1}{1000} + \frac{0 - V_o}{10000} = 0$$

$$\text{From this, } V_o = -10 \text{ v.}$$

However, the op-amp is only supplied $\pm 5\text{v}$, so it will be driven into saturation.

$$\text{so } V_o = -5 \text{ v}$$

(g)



The voltages are

$$\bar{V}_R = 100 \angle 0^\circ \text{ v}$$

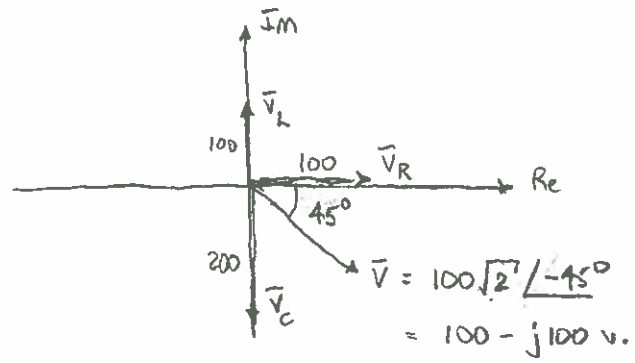
$$\bar{V}_C = -j200 = 200 \angle -90^\circ \text{ v}$$

$$\bar{V}_L = j100 = 100 \angle 90^\circ \text{ v}$$

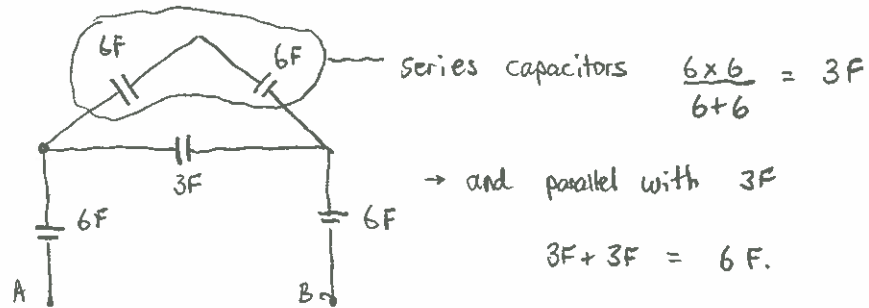
$$\text{And the total voltage } \bar{V} = \bar{V}_R + \bar{V}_C + \bar{V}_L$$

$$= 100 - j200 + j100 = 100 - j100 \text{ v.}$$

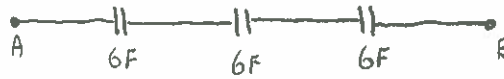
Phasor diagram



(h)



This simplifies to



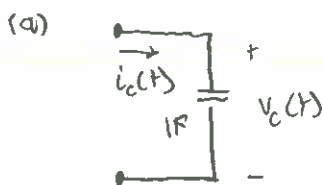
Three series capacitors

$$C_{AB} = \left(\frac{1}{6} + \frac{1}{6} + \frac{1}{6} \right)^{-1}$$

$$= \left(\frac{3}{6} \right)^{-1}$$

$C_{AB} = 2F$

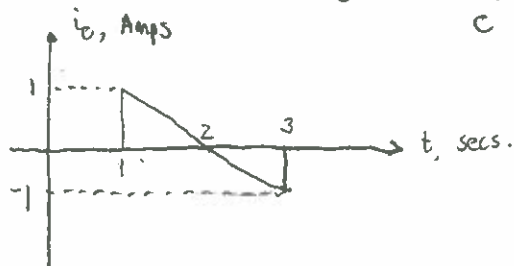
Problem 2



For the capacitor, $i_c(t) = C \frac{dv_c(t)}{dt}$

We are given a waveform for $i_c(t)$, so solve for $v_c(t)$

$$v_c(t) = \frac{1}{C} \int_0^t i_c(\tau) d\tau + v_c(0)$$



This line has slope $\frac{1 - (-1) \text{ A}}{1 - 3 \text{ secs}} = -1$

The equation of the line between $t=1$ and $t=3$

$$i_c(t) = -t + i_0$$

The intercept i_0 can be calculated from any point on the line. At $t=2$, $i_c(t) = 0$

$$i_c(t) = 0 = -2 + i_0, \text{ so } i_0 = 2 \text{ A.}$$

Therefore, $i_c(t) = -t + 2$.

The voltage on the capacitor by interval:

$t < 1 \text{ s}$: $V_c(t) = 0$

$1 \leq t \leq 3$: $V_c(t) = \frac{1}{C} \int_1^t (-\tau + 2) d\tau = \left. -\frac{\tau^2}{2} + 2\tau \right|_1^t$

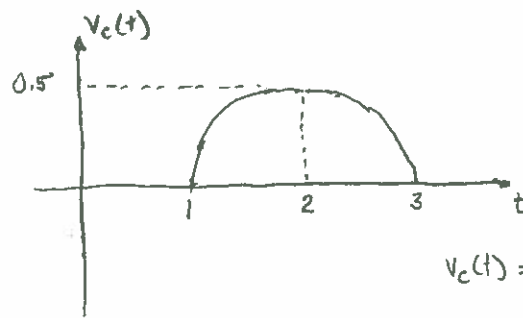
$$V_c(t) = -\frac{t^2}{2} + 2t - \left(-\frac{1}{2} + 2 \right)$$

so $V_c(t) = -\frac{t^2}{2} + 2t - 1.5 \text{ v.}$

$t > 3$: Evaluating the above equation at $t=3$,

$$V_c(3) = -\frac{(3)^2}{2} + 2(3) - 1.5 = -4.5 + 6 - 1.5$$

so $V_c(t) = 0 \text{ v.}$



$$V_c(2) = -\frac{2^2}{2} + 2(2) - 1.5 \\ = 0.5 \text{ v.}$$

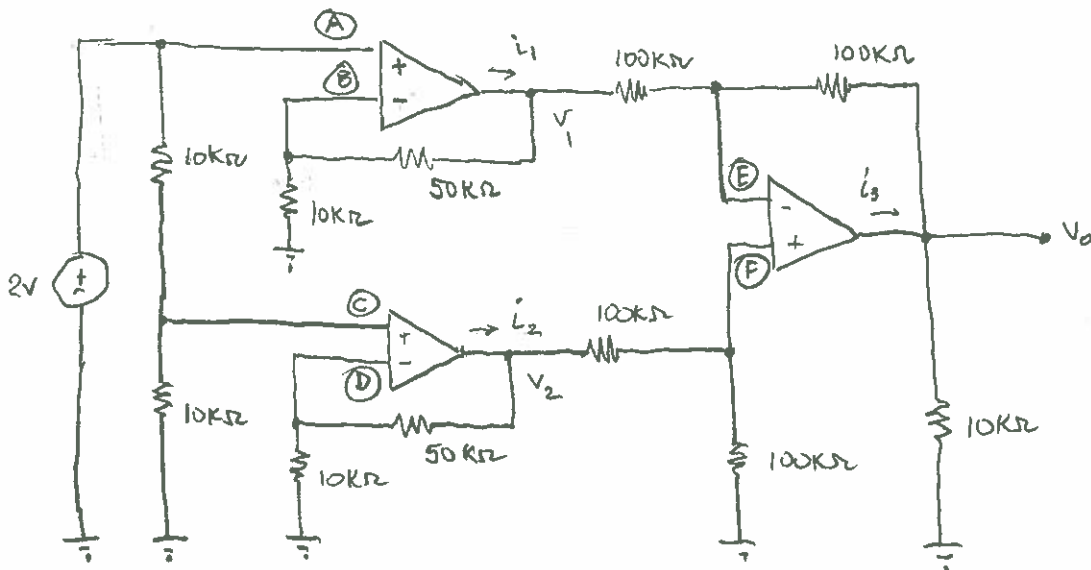
$$V_c(t) = 0 \text{ for } 0 \leq t < 1, \\ 3 \leq t < 4.$$

(b) Power in capacitor: $P_c(t) = V_c(t) i_c(t)$

$$P_c(t) = \left(-\frac{t^2}{2} + 2t - 1.5\right)(-t + 2) \\ = \frac{t^3}{2} - 2t^2 + 1.5t - 2\frac{t^2}{2} + 4t - 3$$

$$P_c(t) = \frac{t^3}{2} - 3t^2 + 5.5t - 3 \text{ W.}$$

Problem 3



(a) At node A, we know $V_A = 2\text{v}$, so $V_B = 2\text{v}$.

$$\text{At node B: } \frac{V_B}{10\text{k}} + \frac{V_B - V_1}{50\text{k}} = 0$$

$$\text{so } \frac{2}{10\text{k}} + \frac{2 - V_1}{50\text{k}} = 0$$

$$\text{giving } 10 + 2 - V_1 = 0$$

$$\boxed{V_1 = 12 \text{ v}}$$

$$\text{At node C: } \frac{V_C}{10\text{K}} + \frac{V_C - 2}{10\text{K}} = 0$$

$$V_C + V_C - 2 = 0, \text{ so } V_C = 1 \text{ v.}$$

$$\text{At node D: } \frac{V_D}{10\text{K}} + \frac{V_D - V_2}{50\text{K}} = 0, \text{ where } V_D = V_C = 1 \text{ v.}$$

$$\frac{1}{10\text{K}} + \frac{1 - V_2}{50\text{K}} = 0$$

$$\text{giving } 5 + 1 - V_2 = 0$$

$$\boxed{V_2 = 6 \text{ v}}$$

$$(b) \text{ At node E: } \frac{V_E - V_1}{100\text{K}} + \frac{V_E - V_0}{100\text{K}} = 0$$

$$V_E - V_1 + V_E - V_0 = 0$$

$$\text{so } 2V_E = V_1 + V_0$$

$$V_0 = -V_1 + 2V_E$$

$$\text{At node F: } \frac{V_F}{100\text{K}} + \frac{V_F - V_2}{100\text{K}} = 0, \text{ where } V_F = V_E$$

$$V_F + V_F - V_2 = 0$$

$$V_F = \frac{1}{2} V_2$$

$$\text{so } V_F = \frac{1}{2}(6) = 3 \text{ v.}$$

Therefore

$$V_0 = -V_1 + 2V_F = -12 + 2(3)$$

$$\boxed{V_0 = -6 \text{ v}}$$

$$(c) \text{ At node } V_1: -i_1 + \frac{V_1 - V_B}{50K} + \frac{V_1 - V_E}{100K} = 0$$

$$\text{We know } V_1 = 12V, V_B = 2V, V_E = 3V$$

$$-i_1 + \frac{12-2}{50K} + \frac{12-3}{100K} = 0$$

$$-(100K)i_1 + 2(12-2) + 12-3 = 0$$

$$-(100K)i_1 + 20 + 9 = 0$$

$$i_1 = \frac{29}{100K} = 0.29 \text{ mA}$$

$$\text{At node } V_2: -i_2 + \frac{V_2 - V_F}{100K} + \frac{V_2 - V_D}{50K} = 0$$

$$\text{We know } V_2 = 6V, V_D = 1V, V_F = 3V.$$

$$-i_2 + \frac{6-3}{100K} + \frac{6-1}{50K} = 0$$

$$-(100K)i_2 + 6-3 + 2(6-1) = 0$$

$$-(100K)i_2 + 3 + 10 = 0$$

$$i_2 = \frac{13}{100K} = 0.13 \text{ mA}$$

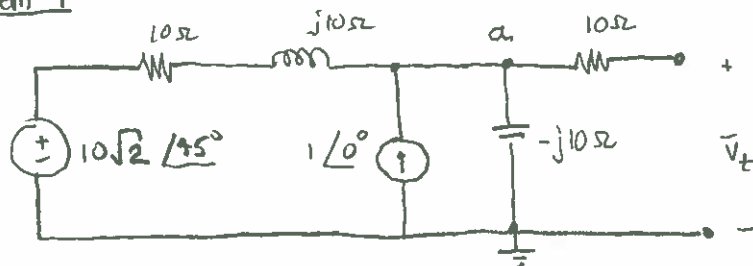
$$\text{At node } V_D: -i_3 + \frac{V_D - V_E}{100K} + \frac{V_D}{10K} = 0$$

$$\text{We know } V_D = -6V, V_E = 3V$$

$$-(100K)i_3 + -6-3 + 10(-6)$$

$$i_3 = \frac{63}{100K} = -0.51 \text{ mA}$$

Problem 4



(a) With the circuit labelled as shown, $\bar{V}_t = \bar{V}_a$

$$\text{At node } a: \frac{\bar{V}_a - 10\sqrt{2} \angle 45^\circ}{10 + j10} - 1 + \frac{\bar{V}_a}{-j10} = 0$$

$$\text{where } 10\sqrt{2} \angle 45^\circ = 10\sqrt{2} \cos(45^\circ) + j10\sqrt{2} \sin(45^\circ) \\ = 10 + j10$$

$$\text{so } \frac{\bar{V}_a - 10 - j10}{10 + j10} - 1 + \frac{\bar{V}_a}{-j10} = 0$$

$$\bar{V}_a \left(\frac{1}{10 + j10} + \frac{1}{-j10} \right) = \frac{10 + j10}{10 + j10} + 1$$

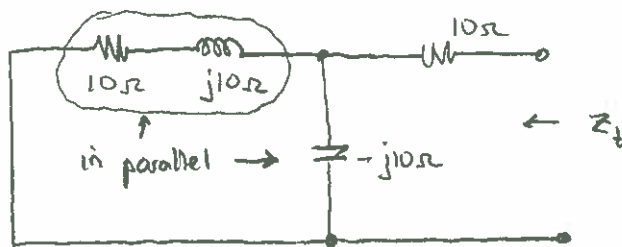
$$\bar{V}_a \left(\frac{-j10 + 10 + j10}{(-j10)(10 + j10)} \right) = 2$$

$$\bar{V}_a \left(\frac{10}{-j100 + 100} \right) = 2$$

$$\text{so } \bar{V}_a = 2(10 - j10) \\ = 20 - j20$$

$$\text{Finally, } \boxed{\bar{V}_t = \bar{V}_a = 20 - j20 = 20\sqrt{2} \angle -45^\circ}$$

(b) There are no dependent sources, so we can zero the sources



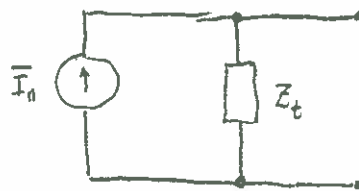
$$\begin{aligned} \text{We have } Z_t &= \frac{(10+j10)(-j10)}{(10+j10-j10)} + 10\Omega \\ &= \frac{-j100 + 100}{10} + 10\Omega \end{aligned}$$

$$Z_t = 10 - j10 + 10$$

$$\text{so } Z_t = 20 - j10\Omega = 22.36 \angle -26.57^\circ$$

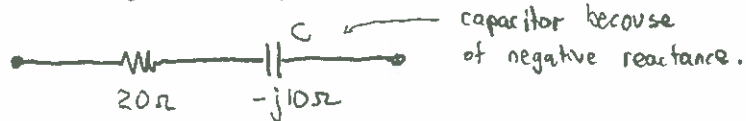
(c) The Norton current is

$$\begin{aligned} \bar{I}_n &= \frac{\bar{V}_t}{Z_t} = \frac{20\sqrt{2} \angle 45^\circ}{22.36 \angle -26.57^\circ} \\ &= 1.265 \angle 71.57^\circ \\ &= 0.396 + j1.2 \end{aligned}$$



NORTON
EQUIVALENT

(d) We have $Z_t = 20 - j10\Omega$



$$Z_t = -j10 = \frac{1}{j\omega C}, \quad \text{where } \omega = 100 \text{ rad/sec}$$

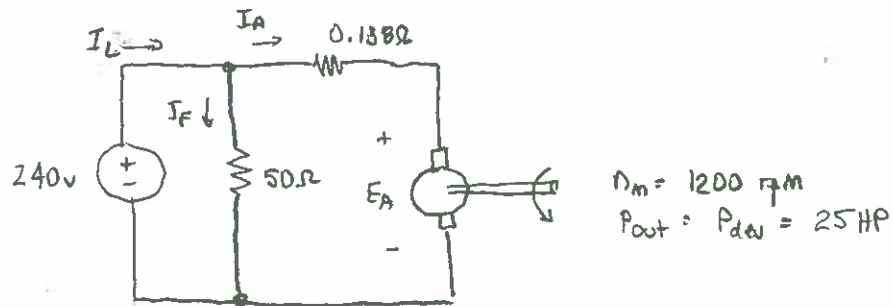
$$\text{so } \omega C = \frac{1}{10}, \quad C = \frac{1}{10\omega} \text{ F}$$

$$C = \frac{1}{10(100)} \text{ F}$$

$$R = 20\Omega, \quad C = 1000 \mu\text{F}$$

Problem 5

(a)



Initially, $n_m = 0$, so the induced voltage E_A

$$E_A = k\phi\omega_m = 0$$

Therefore, the initial armature current $I_A = \frac{V_T}{R_A}$

$$I_A = \frac{240}{0.138} = 1739.1 \text{ A}$$

(b) Since there are no rotational losses, $P_{dev} = P_{out}$

$$P_{out} = 25 \times 746 = 18,650 \text{ W.}$$

The output torque $T_{out} = T_{dev}$

$$T_{out} = \frac{P_{out}}{\omega_m} = \frac{18,650}{1200 \times \frac{2\pi}{60}} = 148.412 \text{ N}\cdot\text{m}$$

We are given the efficiency $\eta = 90\%$, so total power input P_{in}

$$P_{in} = \frac{P_{out}}{\eta} = \frac{18,650}{0.9} = 20,722.2 \text{ W}$$

This means that $P_{in} = V_T I_L$, so $I_L = \frac{20,722.2}{240}$

$$I_L = 86.34 \text{ A}$$

KCL gives $I_L = I_F + I_A = \left(\frac{V_T}{R_F}\right) + I_A$

$$\text{so } I_A = 86.34 - \frac{240}{50} = 81.54 \text{ A}$$

Armature and field losses :

$$P_F = \frac{V_T^2}{R_F} = \frac{(240)^2}{50} = 1152 \text{ W}$$

$$P_A = I_A^2 R_A = (81.54)^2 (0.138) = 917.53 \text{ W}$$

Back EMF: $E_A = V_T - I_A R_A$
 $= 240 - (81.54)(0.138) = 228.7 \text{ V}$

Summary :

$T_{\text{out}} = 148.412 \text{ N-m}$ $P_A = 917.53 \text{ W}$ $P_F = 1152 \text{ W}$ $E_A = 228.7 \text{ V}$

(c) From the above information, we can find the machine constant.

$$K\phi = \frac{T_{\text{dev}}}{I_A} = \frac{148.412}{81.54} = 1.82$$

with $T_{\text{dev}} = 100 \text{ N-m}$, the new I_A is

$$I_A = \frac{T_{\text{dev}}}{K\phi} = \frac{100}{1.82} = 54.94 \text{ A}$$

Then $E_A = V_T - I_A R_A = 240 - (54.94)(0.138)$
 $= 232.4 \text{ V}$

The new speed therefore :

$$\omega_m = \frac{E_A}{K\phi} = \frac{232.4}{1.82} = 127.7 \text{ rads/sec}$$

$$\Omega_m = \omega_m \times \frac{60}{2\pi} = 127.7 \times \frac{60}{2\pi}$$

$\Omega_m = 1219 \text{ rpm}$
