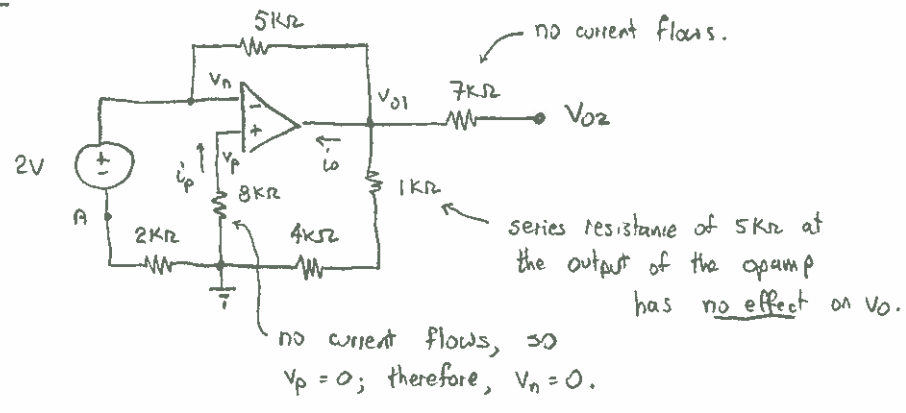


Question 1

(a)



One way to solve this is by recognizing a supernode between nodes \$V\_n\$ and A

Supernode:  $\frac{V_A}{2K} + \frac{V_n - V_{o1}}{5K} + \overset{0}{i_n} = 0$ , where  $V_n = 0$

(x 5K)  $2.5 V_A + 0 - V_{o1} = 0$   
 $V_{o2} = 2.5 V_A$

Supernode dependence:  $V_n - V_A = 2$   
 $0 - V_A = 2 \quad \therefore V_A = -2$

therefore,  $V_{o1} = -5V$ .

Another way is to write a combined equation at node \$V\_n\$

$\frac{V_n - 2}{2K} + \frac{V_n - V_{o1}}{5K} + \overset{0}{i_n} = 0 \Rightarrow \frac{-2}{2K} - \frac{V_{o1}}{5K} = 0$   
 so  $V_{o1} = -5V$

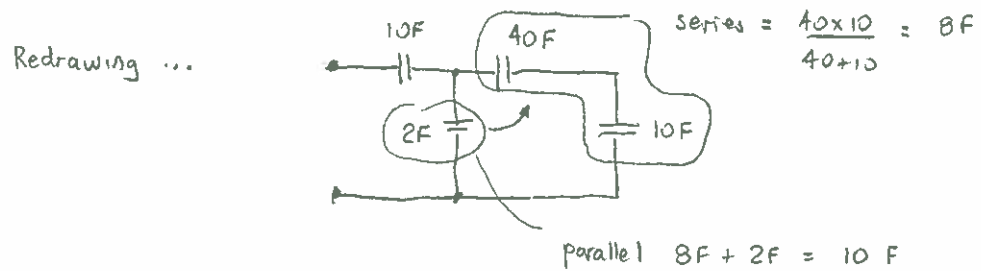
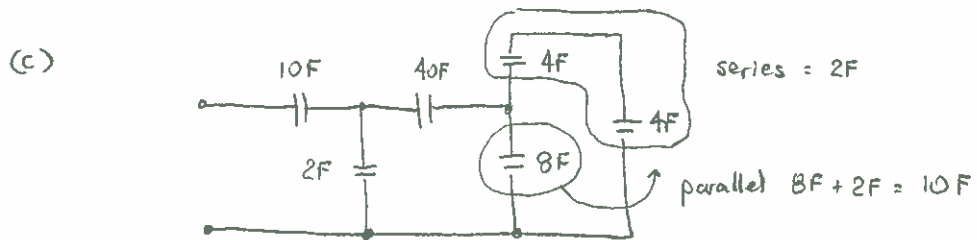
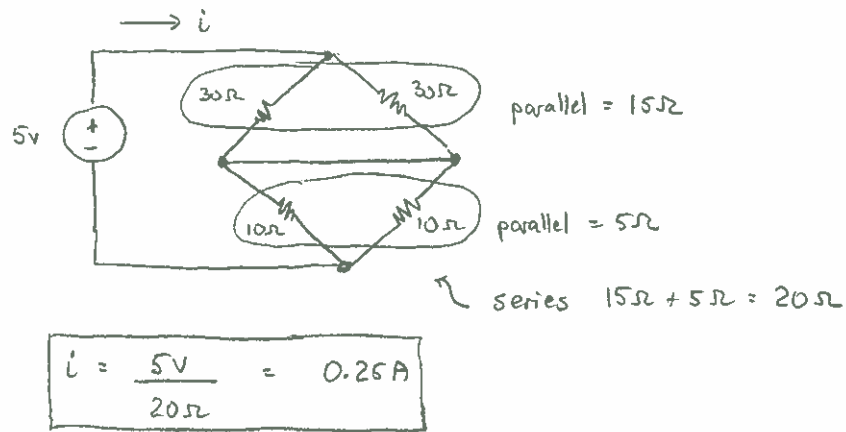
Since there is no current in the output 7kΩ resistor,  $V_{o2} = V_{o1} = -5V$

At node \$V\_{o1}\$,  $\frac{V_{o1} - V_n}{5K} + \frac{V_{o1}}{5K} + i_o = 0$

$\frac{-5 + -5}{5K} = -i_o$ , so  $i_o = 2mA$

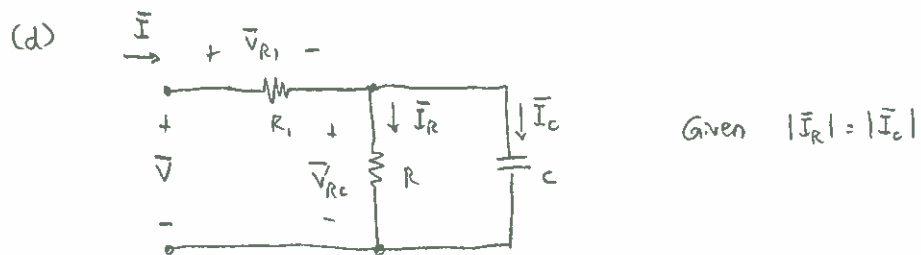
(b) Since the source is DC, the inductor is a short circuit and the capacitor is an open circuit, Redrawing ...





Finally, 10F in series with 10F

$$C_{eq} = 5F$$

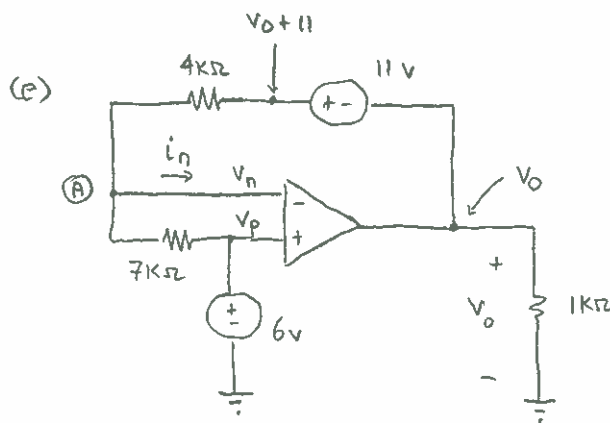
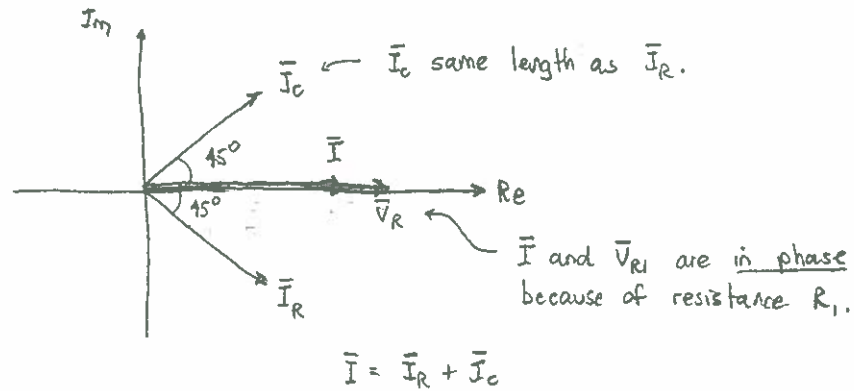


Current  $\bar{I}_R = \frac{\bar{V}_{Rc}}{R}$  and  $\bar{I}_C = \frac{\bar{V}_{Rc}}{1/j\omega C} = (j\omega C)\bar{V}_{Rc}$

so  $\bar{I}_C$  leads  $\bar{I}_R$  by  $90^\circ$

Since we are told that the angle of  $\bar{V}_{R1}$  is  $0^\circ$ , this is also the angle of  $\bar{I}$ .

The imaginary components of  $\bar{I}_R$  and  $\bar{I}_C$  must therefore cancel.



Because  $V_p = 6$ ,  $V_n$  must also be 6v. Then, at node A,

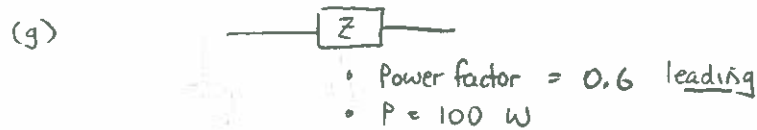
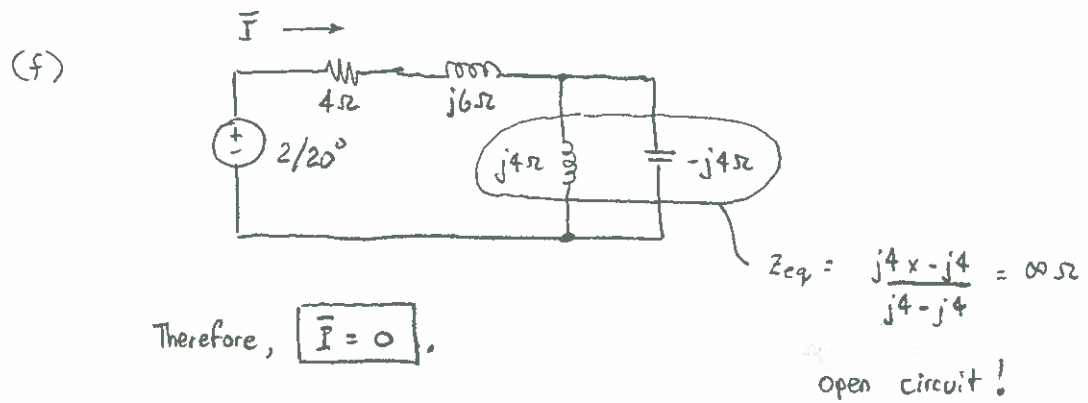
$$\frac{V_A - V_p}{7k} + \cancel{i_n} + \frac{V_A - (V_0 + 11)}{4k} = 0$$

$$\text{where } V_A = V_p = V_n = 6v$$

$$\text{so } \frac{V_A - (V_0 + 11)}{4k} = 0$$

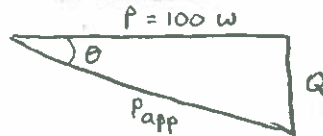
$$V_0 = V_A - 11 = 6 - 11$$

$$\boxed{V_0 = -5v}$$



Current leads voltage, suggesting a capacitive load because  $\theta_I > \theta_V$ . Therefore,  $\theta = \theta_V - \theta_I$  is negative.

Power triangle

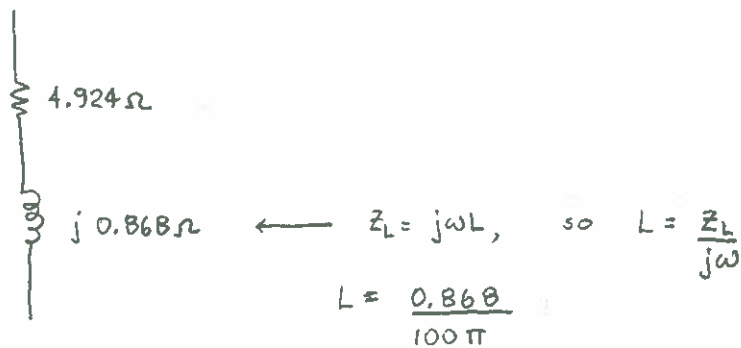


$$P_{app} = \frac{100}{\cos(\theta)} = \frac{100}{0.6} = 166.67 \text{ VA}$$

(h) We know  $\bar{V} = 10 \angle -20^\circ$  and  $\bar{I} = 2 \angle -30^\circ$

$$\text{so } Z = \frac{\bar{V}}{\bar{I}} = 5 \angle 10^\circ, \text{ or } Z = 4.924 + j0.868 \Omega$$

This is a resistor and inductor in series



$$L = 2.76 \text{ mH}$$

Question 2

(a) For the inductor,  $v(t) = L \frac{di(t)}{dt}$

Interval  $0 \leq t \leq 1$  second:  $i(t) = 0$ , so  $v(t) = 0$

For  $1 \leq t \leq 3$ ,  $i(t)$  is a straight line with slope

$$\text{slope} = \frac{10 \text{ A}}{2 \text{ secs}} = 5$$

$$\text{so } v(t) = L \frac{di(t)}{dt} = 4 \times 5 = 20 \text{ V}$$

For  $t > 3$ ,  $i(t)$  is a flat line at 10 A, with zero slope

$$v(t) = 4 \times 0 = 0 \text{ V}$$

For the capacitor,  $i(t) = C \frac{dv(t)}{dt}$ , so  $v(t) = \frac{1}{C} \int_{t_1}^{t_2} i(t) dt + v(t_1)$

For  $0 \leq t \leq 1$ ,  $i(t) = 0$ ,

$$\text{so } v(t) = \frac{1}{2} \int_0^1 0 dt + v(0) = -1 \text{ V}$$

For  $1 \leq t \leq 3$ , we need the equation of the line.

$$i(t) = \underset{\substack{\uparrow \\ \text{slope}}}{5t} - \underset{\substack{\uparrow \\ \text{intercept}}}{5}$$

$$\begin{aligned} \text{so } v(t) &= \int_1^t i(t) dt + v(1) \\ &= \frac{1}{2} \int_1^t (5t - 5) dt + -1 \end{aligned}$$

$$v(t) = \frac{1}{2} \left( \frac{5}{2} t^2 - 5t \right) \Big|_1^t + -1$$

$$\begin{aligned} v(t) &= \frac{5}{4} t^2 - \frac{5}{2} t - \left( \frac{5}{4} - \frac{5}{2} \right) + -1 \\ &= \frac{5}{4} t^2 - \frac{5}{2} t + \frac{1}{4} \end{aligned}$$

For  $t > 3$ ,  $i(t) = 10$ , so

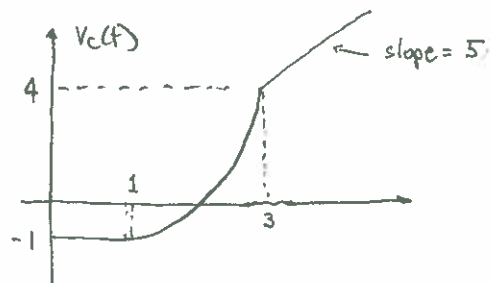
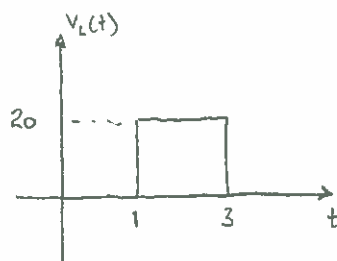
$$v(t) = \frac{1}{2} \int_3^t 10 dt + v(3)$$

$$v(3) = \frac{5}{4}(3)^2 - \frac{5}{2}(3) + \frac{1}{4} = 4$$

$$v(t) = 5t \Big|_3^t + 4$$

$$= 5t - 15 + 4 = 5t - 11$$

Sketch:



(b) Power in the inductor:  $P_L(t) = v_L(t) i(t)$

Interval  $0 \leq t \leq 1$ :  $P_L(t) = 0$

$1 \leq t \leq 3$ :  $P_L(t) = 20 \times (5t - 5)$   
 $= 100t - 100$  W

$t > 3$ :  $P_L(t) = 0$

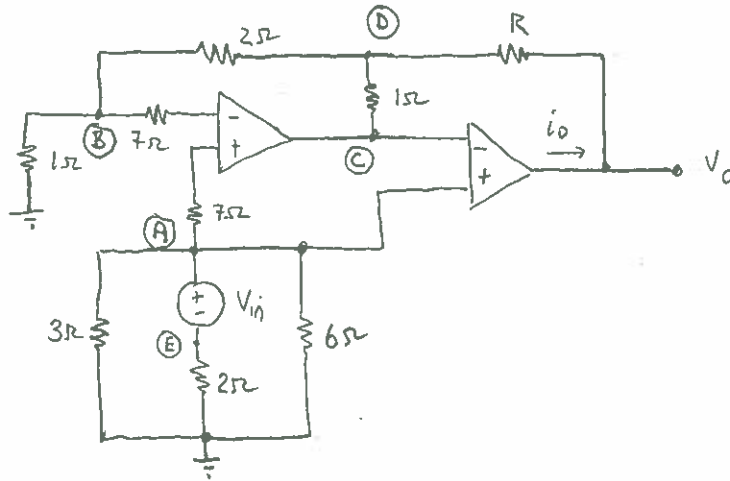
Power in the capacitor:  $P_C(t) = v_C(t) i(t)$

$0 \leq t < 1$ :  $P_C(t) = 0$

$1 \leq t < 3$ :  $P_C(t) = \left( \frac{5}{4}t^2 - \frac{5}{2}t + \frac{1}{4} \right) (5t - 5)$   
 $= \frac{25}{4}t^3 - \frac{25}{2}t^2 + \frac{5}{4}t - \frac{25}{4}t^2 + \frac{25}{2}t - \frac{5}{4}$   
 $= \frac{25}{4}t^3 - \frac{75}{4}t^2 + \frac{55}{4}t - \frac{5}{4}$  W

$t \geq 3$ :  $P_C(t) = 10 \times (5t - 11) = 50t - 110$  W.

## Question 3



(a) At node A,  $\frac{V_A}{3} + \frac{V_A}{6} + \frac{V_E}{2} = 0$  (supernode equation)  
 (x6)  $2V_A + V_A + 3V_E = 0$

Dependence:  $V_A - V_E = V_{in}$ , so  $V_E = V_A - V_{in}$

and  $2V_A + V_A + 3(V_A - V_{in}) = 0$   
 $6V_A - 3V_{in} = 0$

so  $V_A = \frac{V_{in}}{2}$

Node B:  $\frac{V_B}{1} + \frac{V_B - V_D}{2} = 0$ , where  $V_B = V_A$   
 $2V_B + V_B = V_D$

so  $V_D = 3V_B = 3V_A = \frac{3}{2}V_{in}$

Node D:  $\frac{V_D - V_O}{R} + \frac{V_D - V_C}{1} + \frac{V_D - V_B}{2} = 0$

where  $V_B = V_A$  and  $V_C = V_A$

$\frac{V_D - V_O}{R} + V_D - V_A + \frac{V_D - V_A}{2} = 0$

$2(V_D - V_O) + 3R(V_D - V_A) = 0$

$2V_D - 2V_O + 3RV_D - 3RV_A = 0$

Substitute  $V_D = \frac{3}{2}V_{in}$  and  $V_A = \frac{1}{2}V_{in}$

$$3V_{in} - 2V_D + \frac{9}{2}RV_{in} - \frac{3}{2}RV_{in} = 0$$

$$3V_{in} + 3RV_{in} = 2V_D$$

$$V_D = \frac{(3 + 3R)V_{in}}{2}$$

(b) Using the answer to (a),  $V_D = \frac{(3 + 3 \cdot 1) \times 6}{2}$   
 $V_D = 18 \text{ V}$

And at node  $V_D$ ,

$$\frac{V_D - V_D}{R} - i_D = 0 \quad \text{where } V_D = \frac{3}{2}V_{in} = 9 \text{ V}$$

$$\text{so } \frac{18 - 9}{1} - i_D = 0$$

$$i_D = 9 \text{ A}$$

(c) The load circuit consists of just a  $2\Omega$  resistor!

$V_D$  will not change:  $V_D = 18 \text{ V}$

And at node  $V_D$ ,  $\frac{V_D - V_D}{R} - i_D + \frac{V_D}{2} = 0$   
load current

$$\frac{18 - 9}{1} - i_D + \frac{18}{2} = 0$$

$$9 + 9 = i_D, \quad \text{so } i_D = 18 \text{ A}$$

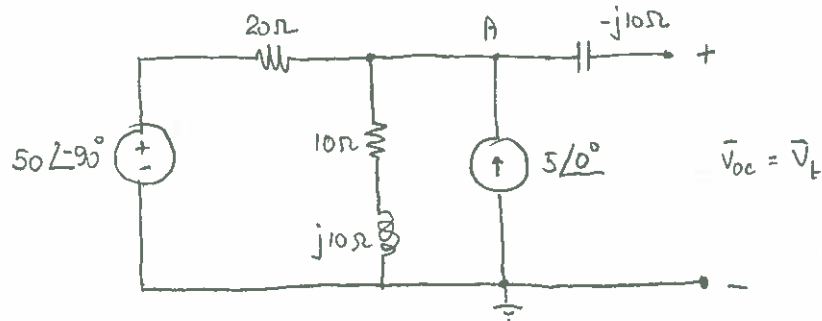


Question 4

(a) With  $\omega = 1000$  r/s,  $Z_L = j\omega L = j(1000)(0.01) = j10\Omega$

and  $Z_C = \frac{1}{j\omega C} = \frac{1}{j(1000)(100 \times 10^{-6})} = -j10\Omega$

(b)



Theremin voltage: Open-circuit voltage will be  $\bar{V}_{oc} = \bar{V}_A$

Node A:  $\frac{\bar{V}_A - 50\angle-90^\circ}{20} + \frac{\bar{V}_A}{10 + j10} - 5\angle 0^\circ = 0$

$$\frac{\bar{V}_A + j50}{20} + \frac{\bar{V}_A}{10 + j10} = 5$$

(x20)  $\bar{V}_A + j50 + \frac{2\bar{V}_A}{1+j} = 100$

(x(1+j))  $(\bar{V}_A + j50)(1+j) + 2\bar{V}_A = 100 + j100$

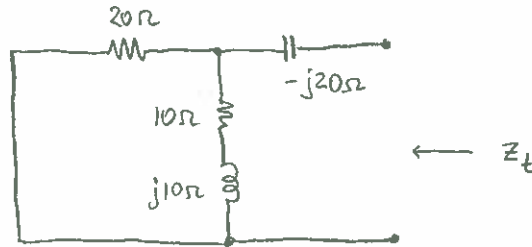
$$\bar{V}_A + j\bar{V}_A + j50 - 50 + 2\bar{V}_A = 100 + j100$$

$$\bar{V}_A(3+j) = 150 + j50$$

$$\bar{V}_A = \frac{150 + j50}{3+j} = \frac{50(3+j)}{3+j}$$

$$\boxed{\bar{V}_A = 50\angle 0^\circ}$$

(c) Since there are no independent sources, we may zero the independent ones



$$Z_t = [20 \parallel (10 + j10)] - j10$$

$$= \frac{20(10 + j10)}{30 + j10} - j10 = \frac{200 + j200}{30 + j10} - j10$$

$$Z_t = \frac{20 + j20}{3 + j} - j10 = \frac{(20 + j20)(3 - j)}{(3 + j)(3 - j)} - j10$$

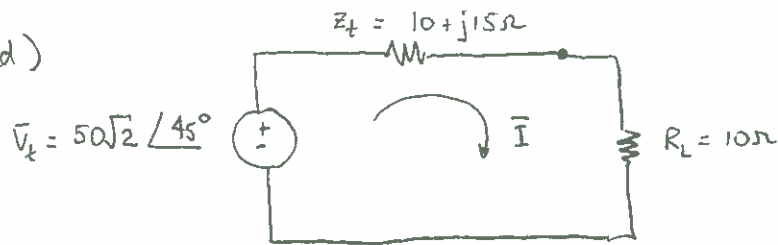
$$= \frac{60 - j20 + j60 + 20}{9 + j3 - j3 + 1} - j10$$

$$= \frac{80 + j40}{10} - j10$$

$$= 8 + j4 - j10$$

$$Z_t = 8 - j6 = 10 \angle -36.87^\circ$$

(d)



$$\bar{I} = \frac{\bar{V}_t}{Z_t + 10} = \frac{50\sqrt{2} \angle 45^\circ}{20 + j15} = \frac{50\sqrt{2} \angle 45^\circ}{25 \angle 36.87^\circ}$$

$$= 2\sqrt{2} \angle 8.13^\circ$$

from this,  $I_{rms} = 2 \text{ A}$

Since the load is purely resistive,

and  $Q = 0 \text{ VAR}$

$$P = I_{rms}^2 \times 10 = 20 \text{ W}$$

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Question 5

(a) From KVL, we know  $E_A = V_T - I_A R_A$

$$= 220 - (18.5)(0.5)$$

$$= 210.75 \text{ V}$$

We know,  $n_m = 1500 \text{ rpm}$ , so  $\omega_m = 1500 \times \frac{2\pi}{60} = 157.08 \text{ rad/s}$

The machine constant:  $E_A = K\phi\omega_m$

$$K\phi = \frac{E_A}{\omega_m} = \frac{210.75}{157.08} = 1.342$$

The developed torque  $T_{dev} = K\phi I_A = 1.342 \times 18.5$

$$T_{dev} = 24.82 \text{ Nm}$$

The total power out is  $P_{out} = 5 \text{ HP} \times 746 = 3730 \text{ W}$

The developed power is  $P_{dev} = T_{dev} \omega_m = 24.82 \times 157.08$

$$= 3898.9 \text{ W}$$

Rotational loss:  $P_{rot} = P_{dev} - P_{out} = 3898.9 - 3730$

$$P_{rot} = 168.9 \text{ W}$$

Armature loss:  $P_A = I_A^2 R_A = (18.5)^2 (0.5)$

$$P_A = 17.11 \text{ W}$$

Field loss:  $P_F = \frac{V_F^2}{R_F} = \frac{(60)^2}{80}$

$$P_F = 45 \text{ W}$$

Efficiency:  $P_{out} = 3730 \text{ W}$ ,  $P_{in} = P_F + V_T I_A$

$$= 45 + (220)(18.5)$$

$$= 4115 \text{ W}$$

$$\eta = \frac{P_{out}}{P_{in}} \times 100\% = 90.6\%$$

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(b) From part (a), the rotational power loss is

$$P_{rot} = 168.9 \text{ W}$$

$$\text{so that } T_{rot} = \frac{P_{rot}}{\omega_m} = \frac{168.9}{157.08} = 1.075 \text{ Nm}$$

$$\text{The armature current } I_A = \frac{T_{rot}}{k\phi} = \frac{1.075}{1.342} = 0.801 \text{ A}$$

$$\begin{aligned} \text{And the new } E_A &= V_T - I_A R_A \\ &= 220 - (0.801)(0.05) \\ &= 219.96 \text{ V.} \end{aligned}$$

$$\text{Therefore, } \omega_m = \frac{E_A}{k\phi} = \frac{219.96}{1.342} = 163.94 \text{ r/s}$$

$$\text{and } n_m = \omega_m \times \frac{60}{2\pi} = \boxed{1565.6 \text{ rpm}}$$

$$(c) \text{ When } n_m = 0 \text{ rpm, } I_A = \frac{V_T - 0}{R_A} = 440 \text{ A}$$

$$\text{so } T_{dev} = k\phi \times 440 = \boxed{590.34 \text{ Nm}}$$

ANSWER