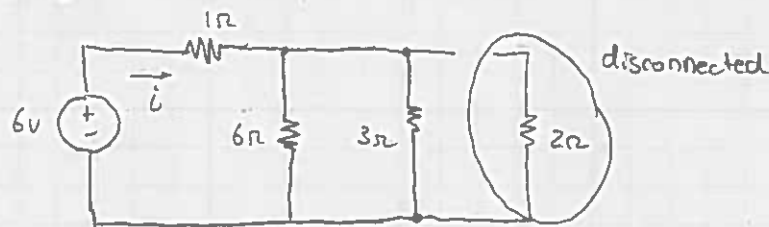


Question 1

- (a) Since the source is DC, the inductor will behave as a short circuit, and the capacitor as open circuit. The circuit simplifies to



Total equivalent resistance: $R_{eq} = 3 // 6 + 1$
 $= 2 + 1 = 3\Omega$

Therefore $i = \frac{6V}{3\Omega} = \boxed{2A}$

- (b) For circuit element x,

- The phasor diagram reveals that current \bar{I} leads voltage \bar{V}_1 by 90°
- For a capacitor, $\bar{I} = \frac{\bar{V}_1}{Z_c \angle -90^\circ} = \bar{V}_1 \times \frac{1}{Z_c} \angle 90^\circ$

so \bar{I} leads \bar{V}_1 by 90° . x is a capacitor

For circuit element y,

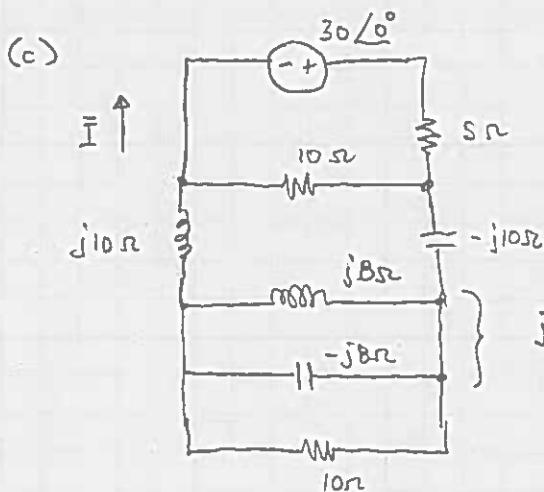
- The phasor diagram reveals that current \bar{I}_y and voltage \bar{V}_2 are in phase, implying that:

y is a resistor. $\bar{V}_2 = R \cdot \bar{I}_y$
↑
real

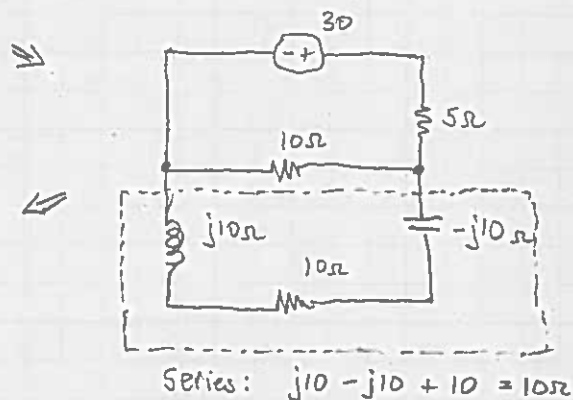
For circuit element z,

- The phasor diagram reveals that the current \bar{I}_z lags the voltage \bar{V}_2 by 90°
- For an inductor, $\bar{I}_z = \frac{\bar{V}_2}{Z_L \angle 90^\circ} = \bar{V}_2 \times \frac{1}{Z_L} \angle -90^\circ$

so \bar{I}_z lags \bar{V}_2 by 90° . z is an inductor



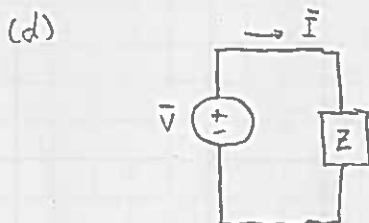
$$\frac{j8 \times -j8}{j8 - j8} = \infty \text{ (open circuit)}$$



This leaves the total equivalent impedance across the source Z_{eq}

$$Z_{eq} = 10 // 10 + 5 = 10\Omega$$

Therefore, $\bar{I} = \frac{30 \angle 0^\circ}{10} = \boxed{3 \angle 0^\circ \text{ A}}$



We have $\bar{S} = \frac{1}{2} \bar{V} \bar{I}^* = 12 \angle 70^\circ$

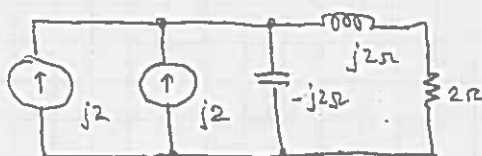
with $\bar{V} = 6 \angle 40^\circ$, $\bar{I}^* = \frac{\bar{S}}{\frac{1}{2} \bar{V}}$

$$\bar{I}^* = \frac{12 \angle 70^\circ}{\frac{1}{2} \times 6 \angle 40^\circ} = 4 \angle 30^\circ$$

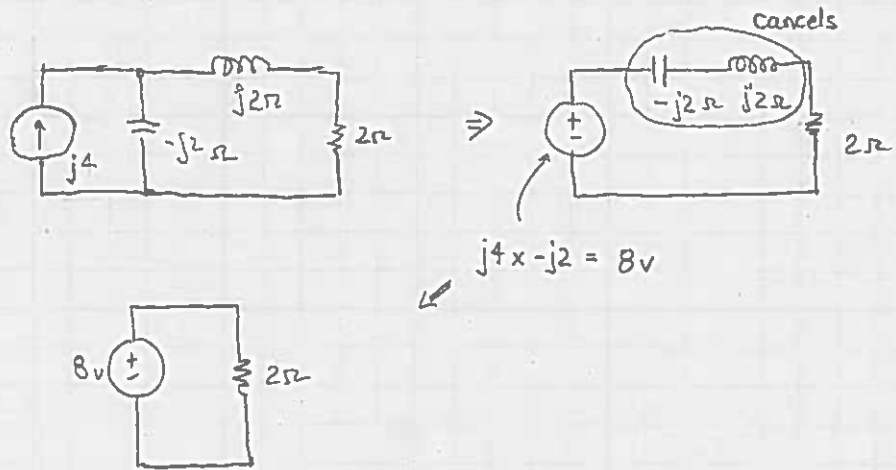
Therefore, $\bar{I} = \boxed{4 \angle -30^\circ}$ and $Z = \frac{\bar{V}}{\bar{I}} = \frac{6 \angle 40^\circ}{4 \angle -30^\circ}$

$$\boxed{1.5 \angle 70^\circ}$$

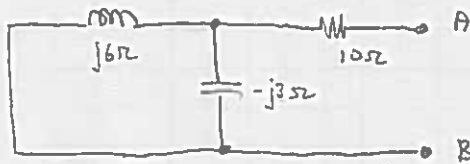
(e) Rearranging the circuit gives



Combining the two current sources ...



(f) Since there are no dependent sources, we may zero the independent ones



$$\begin{aligned} \text{We have } Z_T &= j6 \parallel -j3 + 10 = \frac{j6 \times -j3}{j6 - j3} + 10 \\ &= \frac{18}{j3} + 10 \end{aligned}$$

$$Z_T = 10 - j6$$

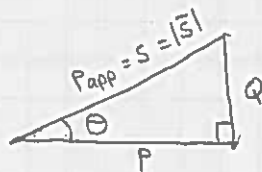
Therefore x (or y) is a 10Ω resistor

$$y \text{ (or } x) \text{ is } \dots -j6 = \frac{-j}{\omega C}$$

$$\text{so } C = \frac{1}{6\omega} = \frac{1}{6 \times 2} = \frac{1}{12} = 0.0833 \text{ F}$$

0.0833 F capacitor

(g) A lagging PF implies a positive power angle (inductive).
The power triangle will look like



We know that $P = 7460 \text{ W}$ and that $\cos(\theta) = 0.7$

Therefore $\theta = +45.57^\circ$

And $\frac{Q}{P} = \tan(\theta)$, so $Q = P \tan(45.57^\circ)$

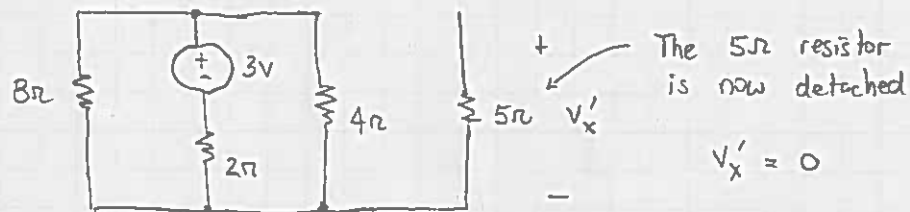
$Q = 7610.7 \text{ VAR}$

Complex power $\bar{S} = P + jQ = 7460 + j7610.7$
 $= 10657 \angle 45.57^\circ \text{ VA}$

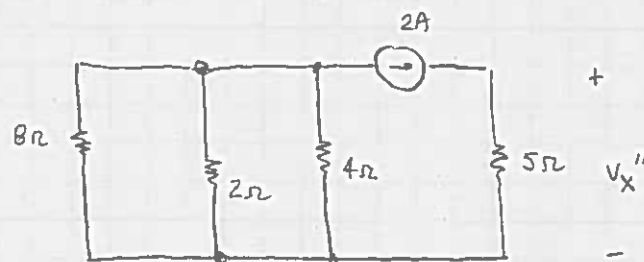
Apparent power $P_{\text{app}} = |\bar{S}| = \sqrt{P^2 + Q^2} = 5$

$P_{\text{app}} = 10657 \text{ VA}$

(h) Consider the voltage source by itself



Now the current source by itself



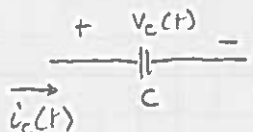
The current in the 5Ω resistor is simply 2A, irrespective of the rest of the circuit.

$$V''_x = 2\text{A} \times 5\Omega = 10\text{V}$$

By superposition, $V_x = V'_x + V''_x$

$V_x = 10\text{V}$

Question 2

(a)  $C = \frac{1}{3} \text{ F}$

During the time interval $0 \leq t < 6$ secs,

$$v_c(t) = \frac{1}{C} \int_0^t i_c(x) dx + v_c(0)$$

During this interval, $i_c(t) = \left(\frac{0.1}{6}\right)t = 0.0667t$

$$\begin{aligned} \text{so } v_c(t) &= 3 \int_0^t 0.0667x dx + 1.4 \\ &= 0.1x^2 \Big|_0^t + 1.4 \end{aligned}$$

$$v_c(t) = 0.1t^2 + 1.4$$

Thus, the voltage is 1.4 V when $t=0$, and reaches a peak of

$$v_c(6) = 0.1(6^2) + 1.4 = 5 \text{ V}$$

The next interval is $6 \leq t < 12$, where

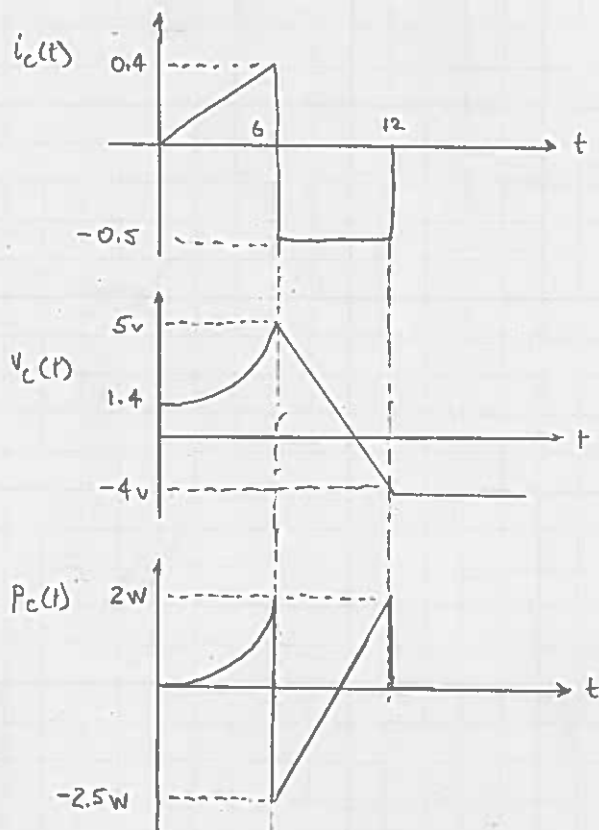
$$i_c(t) = -0.5 \text{ A}$$

$$\begin{aligned} \text{Then, } v_c(t) &= 3 \int_6^t (-0.5) dx + v_c(6) \\ &= -1.5x \Big|_6^t + 5 \\ &= -1.5(t-6) + 5 \\ &= -1.5t + 9 + 5 \\ &= -1.5t + 14 \end{aligned}$$

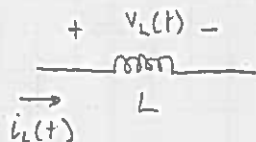
This evaluates to $v_c(6) = -9 + 14 = 5$ and $v_c(12) = -18 + 14 = -4 \text{ V}$.

Finally, for $t \geq 12$, $i_c(t) = 0$, and the capacitor maintains a constant voltage of $v_c(12) = -4 \text{ V}$.

Sketching the resulting voltage and power waveforms ...



(b)



$$L = 0.2 \text{ H}$$

During the interval $0 \leq t < 4$, $i_L(t)$ has a slope of $20/4 = 5$.

$$\text{Therefore } v_L(t) = L \frac{di_L(t)}{dt} = 0.2 \times 5 = 1 \text{ V}$$

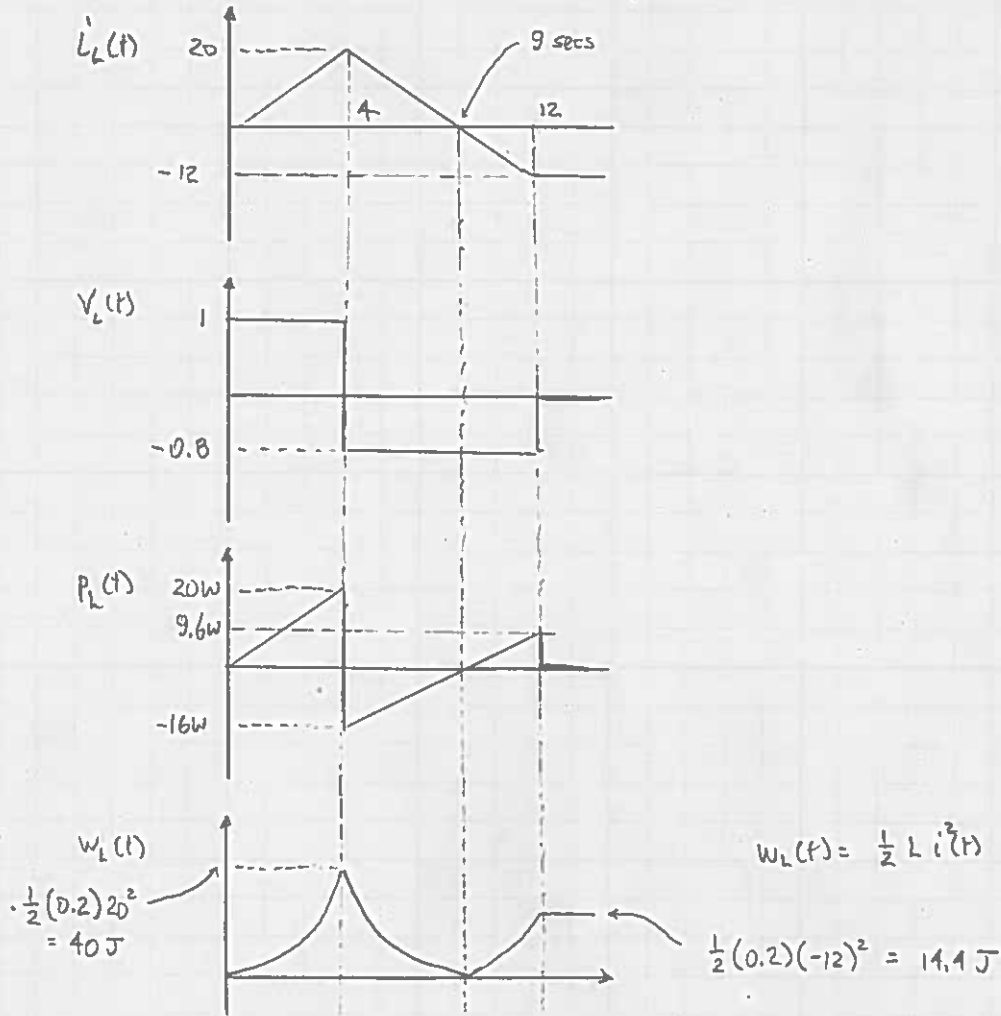
During the next interval $4 \leq t < 12$, $i_L(t)$ has a slope m

$$m = \frac{-12 - 20}{12 - 4} = -4$$

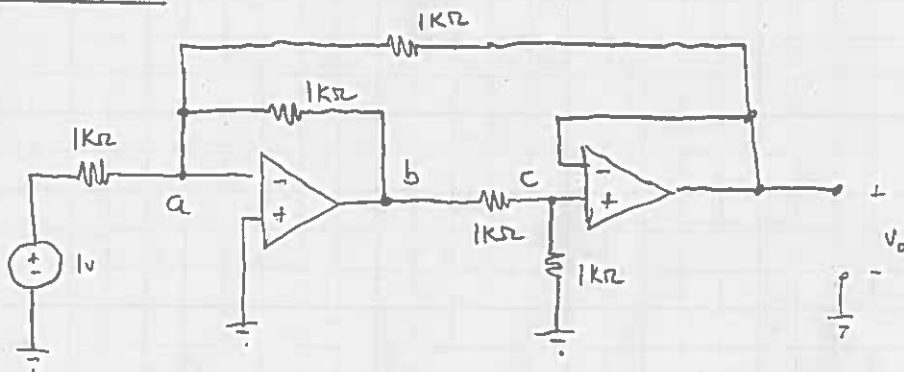
$$\text{so that } v_L(t) = 0.2 \times -4 = -0.8 \text{ V}$$

Finally, for $t \geq 12$, slope = 0 and $v_L(t) = 0$

Sketching the resulting voltage, power, and energy waveforms ..



Question 3



The node-voltage method gives:

$$\text{Node a: } \frac{V_a - 1}{1000} + \frac{V_a - V_b}{1000} + \frac{V_a - V_o}{1000} = 0$$

We know $V_a = 0$, so

$$0 - 1 + 0 - V_b + 0 - V_o = 0$$

$$V_o + V_b = -1 \quad (1)$$

Node c: $\frac{V_c - V_b}{1000} + \frac{V_c}{1000} = 0$

$$2V_c = V_b \quad (2)$$

We also know that $V_c = V_o$ from the second op-amp, so equation (2) becomes

$$V_b = 2V_o$$

Substitute into (1) $V_o + 2V_o = -1$

$$V_o = -\frac{1}{3} \text{ V}$$

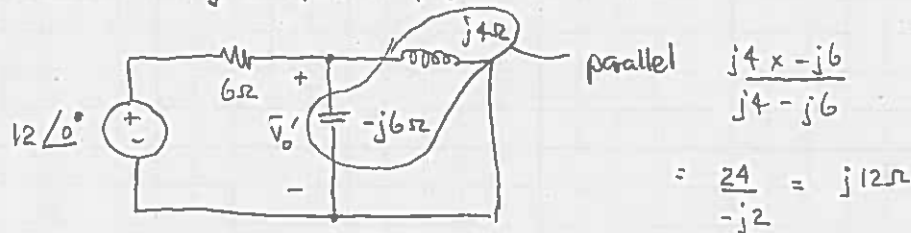
Question 4

Impedances in the circuit for $\omega = 2 \text{ rads/sec}$

inductor: $Z_L = j\omega L = j \times 2 \times 2 \text{ H} = j4\Omega$

capacitor: $Z_C = \frac{1}{j\omega C} = \frac{1}{j \times 2 \times \frac{1}{2}} = -j6\Omega$

The circuit with just $V_1(t)$ is play



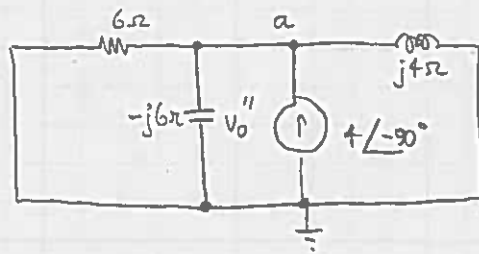
Then, by voltage division $\bar{V}'_0 = \frac{j12}{6 + j12} \times 12$

$$\bar{V}'_0 = \frac{j2}{1 + j2} \times \frac{1 - j2}{1 - j2} \times 12$$

$$\bar{V}'_0 = \frac{j2 + 4}{1 - j2 + j2 + 4} \times 12 = \frac{48 + j24}{5} = 9.6 + j4.8$$

or $10.73 \angle 26.56^\circ$

The circuit with just $i_1(t)$ energized



Node-voltage method: Node a: $\frac{\bar{V}_a}{6} + \frac{\bar{V}_a}{-j6} + \frac{\bar{V}_a}{j4} - 4\angle -90^\circ = 0$

$$(\times 24) \quad \bar{V}_a(4 + j4 - j6) = 96\angle -90^\circ$$

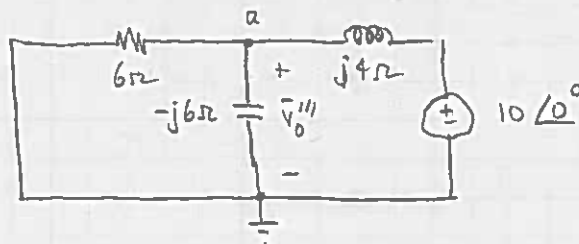
$$\bar{V}_a(4 - j2) = -j96$$

$$\bar{V}_a = \frac{-j96}{4 - j2} = \frac{-j48}{2 - j} \times \frac{2 + j}{2 + j}$$

$$\bar{V}_a = \frac{-j96 + 48}{4 - 2j + 2j + 1} = \frac{-j96 + 48}{5}$$

$$\text{so } \bar{V}_0'' = \bar{V}_a = 9.6 - j19.2 = 21.47\angle -63.4^\circ$$

Finally, with just $v_2(t)$



At node a: $\frac{\bar{V}_a}{6} + \frac{\bar{V}_a}{-j6} + \frac{\bar{V}_a - 10}{j4} = 0$

$$(24) \quad 4\bar{V}_a + j4\bar{V}_a - j6\bar{V}_a + j60 = 0$$

$$\bar{V}_a(4 + j4 - j6) = -j60$$

$$\bar{V}_a(4 - j2) = -j60$$

$$\text{so } \bar{V}_a = \frac{-j60}{4 - j2} = \frac{-j30}{2 - j} \times \frac{2 + j}{2 + j} = \frac{-j60 + 30}{4 + j2 - j2 + 1}$$

$$\bar{V}_0''' = \bar{V}_a = \frac{-j60 + 30}{5} = 6 - j12 = 13.42\angle -63.43^\circ$$

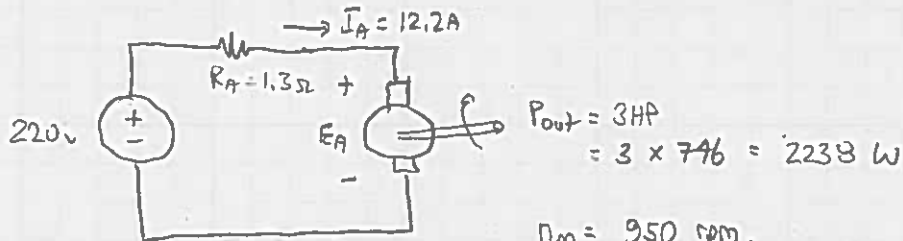
Finally,

$$V_0 = V_0' + V_0'' + V_0''' = (9.6 + j4.8) + (9.6 - j19.2) + (6 - j12)$$

$$= 25.2 - j26.4 = \boxed{36.50\angle -46.33^\circ}$$

Question 5

(a) In the armature circuit, at full load.



$$n_m = 950 \text{ rpm,}$$

$$\text{so } \omega_m = 2\pi \frac{950}{60} = 99.484 \text{ rad/s}$$

By KVL, $E_A = 220 - I_A R_A$

$$= 220 - (12.2)(1.3) = 204.14 \text{ V}$$

$$P_{dev} = I_A E_A = (12.2)(204.14) = \boxed{2490.508 \text{ W}}$$

And $T_{dev} = P_{dev} / \omega_m = 2490.508 / 99.484 = \boxed{25.034 \text{ Nm}}$

The armature power loss is $P_A = I_A^2 R_A$

$$= (12.2)^2 (1.3) = \boxed{193.492 \text{ W}}$$

Rotational power losses will be $P_{rot} = P_{dev} - P_{out}$

$$= 2490.508 - 2238$$

$$P_{rot} = \boxed{252.508 \text{ W}}$$

(b) Removing the mechanical load leaves only the rotational losses as the developed torque.

$$T_{rot} = P_{rot} / \omega_m = 252.508 / 99.484$$

$$= 2.538 \text{ Nm}$$

From part (a), we may determine the machine constant

$$k\phi = \frac{E_A}{\omega_m} = \frac{204.14}{99.484} = 2.052$$

The new armature current is $I_A = \frac{T_{dev}}{k\phi} = \frac{T_{rot}}{k\phi}$

$$I_A = \frac{2.538}{2.052} = 1.237 \text{ A}$$

$$\text{And } E_A = 220 - I_A R_A = 220 - (1.237)(1.3) \\ = 218.392 \text{ V}$$

$$\text{Therefore, } \omega_m = \frac{E_A}{K\phi} = \frac{218.392}{2.052} = 106.43 \text{ r/s}$$

$$\text{so } n_m = 60 \times \omega_m / 2\pi = \boxed{1016.3 \text{ rpm}}$$

(c) Halving I_f causes the machine constant to halve

$$\text{New } K\phi = 1.026$$

Neither the output torque nor rotational torque loss change, so the total developed torque is unchanged from part (a)

$$T_{dev} = 25.034 \text{ Nm}$$

$$\text{The new armature current } I_A = \frac{T_{dev}}{K\phi} = \frac{25.034}{1.026} = 24.4$$

$$\text{Giving a new } E_A = 220 - I_A R_A = 188.28 \text{ V}$$

$$\text{and } \omega_m = \frac{E_A}{K\phi} = \frac{188.28}{1.026} = 183.51 \text{ r/s}$$

$$\text{From part (a) } T_{out} = P_{out} / \omega_m = 2238 / 99.484 \\ = 22.496 \text{ Nm}$$

$$\text{Finally, } P_{out} = T_{out} \omega_m = (22.496)(183.51) \\ = 4128.27 \text{ W}$$

$$P_{out} = \boxed{5.534 \text{ HP}}$$