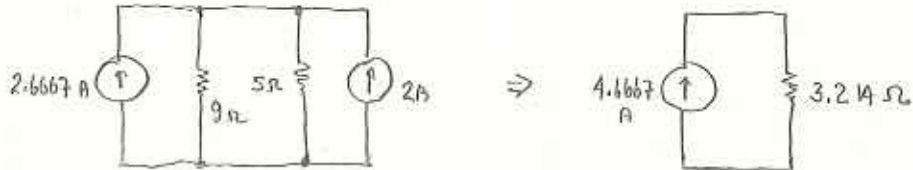
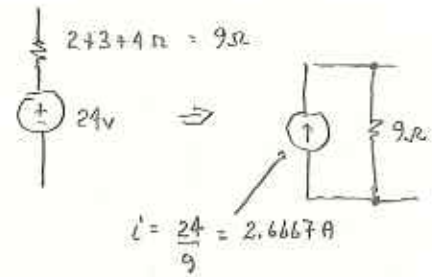
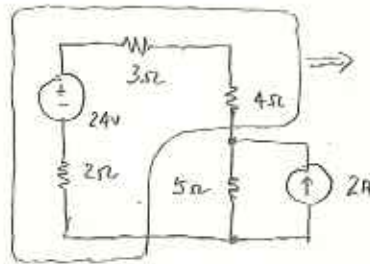
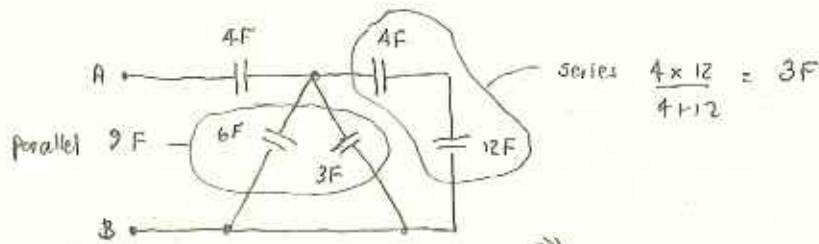


Question 1.

(a)

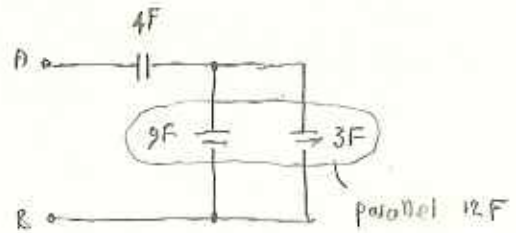


(b)

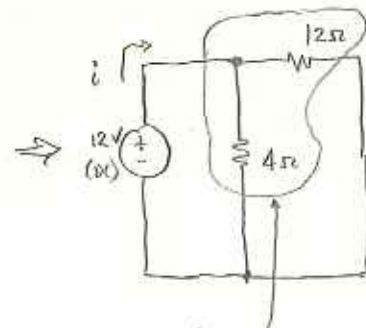
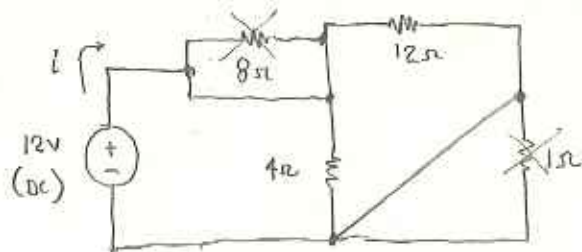


Series $\frac{4 \times 12}{4 + 12} = 3 \text{ F}$

$C_{eq} = \frac{4 \times 12}{4 + 12} = 3 \text{ F}$



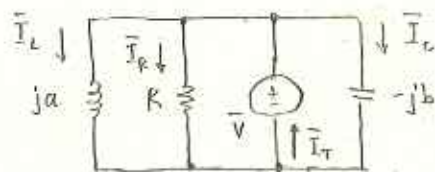
(c) For DC, capacitors look like open circuits and inductors look like a short circuit



parallel $\frac{12 \times 4}{12 + 4} = 3 \Omega$

So $i = \frac{12 \text{ V}}{3 \Omega} = 4 \text{ A}$

(d)



Since $a=b$, the inductor and capacitor are in parallel resonance.
We have

$$\bar{I}_L = \frac{\bar{V}}{ja}, \quad \bar{I}_C = \frac{\bar{V}}{-jb}, \quad \bar{I}_R = \frac{\bar{V}}{R}$$

$$\text{and } \bar{I}_T = \bar{I}_L + \bar{I}_C + \bar{I}_R = \frac{\bar{V}}{ja} - \frac{\bar{V}}{jb} + \frac{\bar{V}}{R}$$

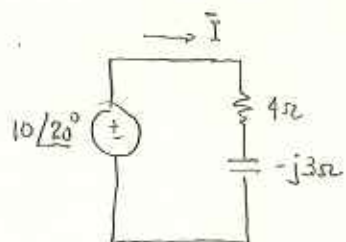
cancels.

$$\bar{I}_T = \bar{I}_R = \frac{\bar{V}}{R}$$

Since the inductor current cancels the capacitor current, the total current is simply the resistor current.

$$\bar{I}_R \text{ and } \bar{I}_T \text{ are in phase, so } \theta = \theta_T - \theta_P = 0^\circ$$

(e)



$$\text{We have } \bar{I} = \frac{10/20^\circ}{4-j3}$$

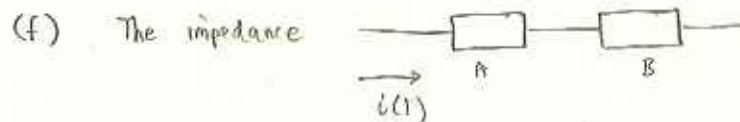
$$\text{or } \bar{I} = \frac{10/20^\circ}{5/-36.87^\circ}$$

$$= 2/56.87^\circ$$

$$\text{Complex power } \bar{S} = \frac{1}{2} \bar{V} \bar{I}^* = \frac{1}{2} (10/20^\circ) (2/-56.87^\circ)$$

$$\bar{S} = 10/-36.87^\circ = \begin{matrix} 8 & - & j6 & \text{VA} \\ \uparrow & & \swarrow & \\ P=8 & & Q=-6 & \end{matrix}$$

The current leads the voltage, so this is a leading power factor.



We are given $v(t) = 10 \sin(100t + 30^\circ) = 10 \cos(100t + 30^\circ - 90^\circ)$

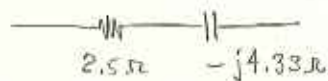
so $\bar{V} = 10 \angle -60^\circ$

and also $i(t) = 2 \cos(100t)$, so $\bar{I} = 2 \angle 0^\circ$

Therefore $Z = \frac{\bar{V}}{\bar{I}} = \frac{10 \angle -60^\circ}{2 \angle 0^\circ} = 5 \angle -60^\circ$

or $Z = 2.5 - j4.33 \Omega$

Therefore,

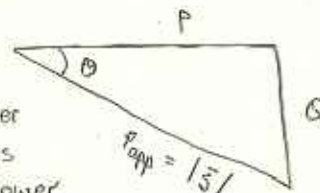


$-j4.33 = \frac{-j}{\omega C}$, $\omega = 100 \text{ rad/s}$

so $C = \frac{1}{4.33 \omega} = \frac{1}{4.33 \times 100}$

$C = 2.3094 \text{ mF}$

(g) The power triangle



leading power factor implies a negative power angle.

The power factor is 0.6, so $\cos(\theta) = 0.6$

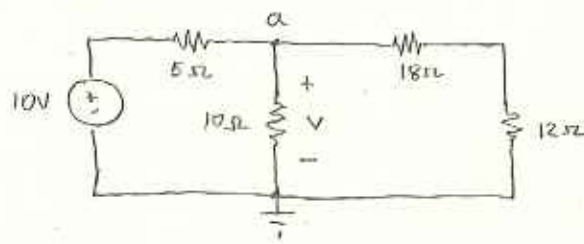
and $\theta = 53.13^\circ$

From the triangle $\cos(\theta) = \frac{P}{P_{app}}$, so $P_{app} = \frac{P}{\cos(\theta)}$

With $P = 6 \text{ W}$, $P_{app} = \frac{6}{0.6} = 10 \text{ VA}$

Question 2

For the voltage source acting alone,



The required voltage is at node a .

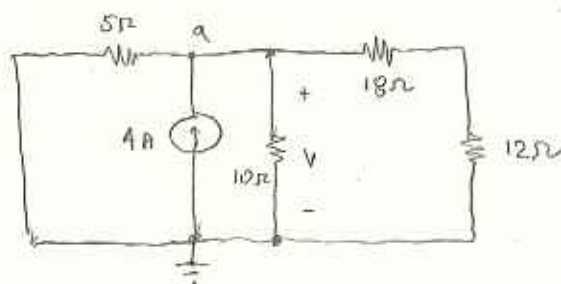
$$\text{Node } a: \frac{V_a - 10}{5} + \frac{V_a}{10} + \frac{V_a}{18+12} = 0$$

$$(x30) \quad 6V_a - 60 + 3V_a + V_a = 0$$

$$10V_a = 60$$

$$\text{so } V_a' = 6\text{V}$$

For the current source alone,



$$\text{Node } a: \frac{V_a}{5} + \frac{V_a}{10} - 4 + \frac{V_a}{30} = 0$$

$$(x30) \quad 6V_a + 3V_a + V_a = 120$$

$$10V_a = 120$$

$$\text{so } V_a'' = 12\text{V}$$

$$\text{By superposition, } V = V_a' + V_a''$$

$$V = 18\text{V}$$

Question 3

For a capacitor, $i = C \frac{dv}{dt}$, so we will be differentiating the voltage graph.

First interval: $0 \leq t < 8$ secs

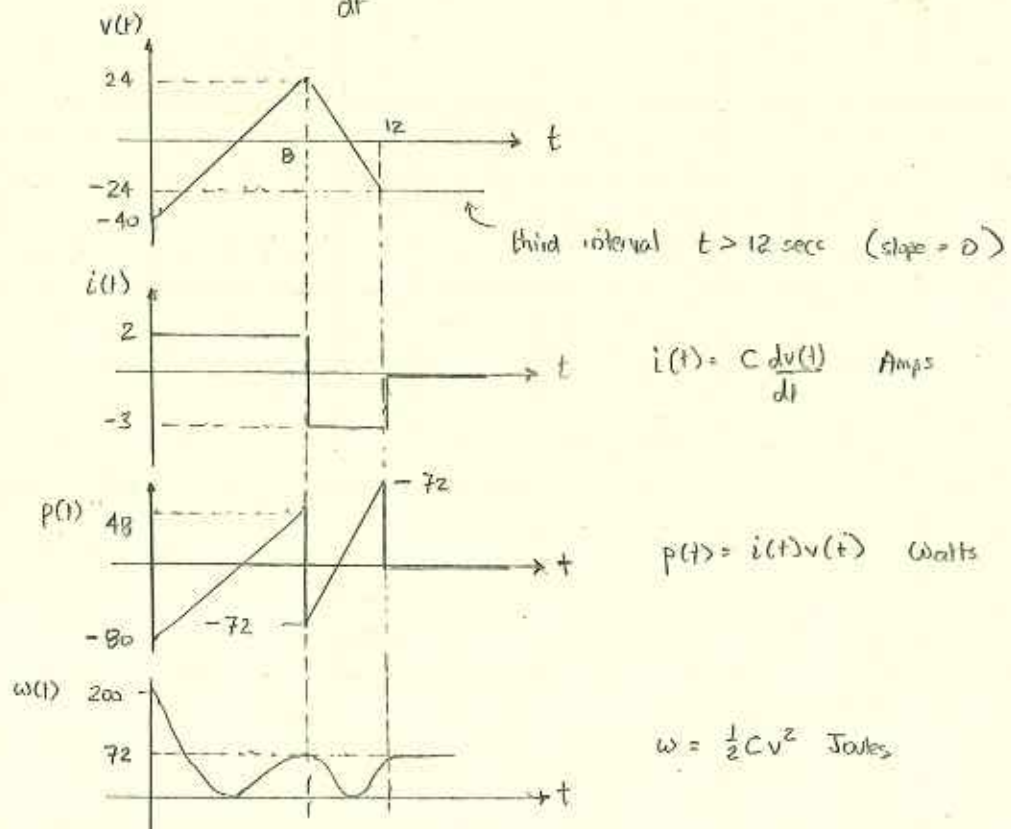
$$\text{slope} = \frac{24 - (-40)}{8} = 8$$

$$\text{so } i = C \frac{dv}{dt} = 0.25 \times 8 = 2 \text{ A (constant)}$$

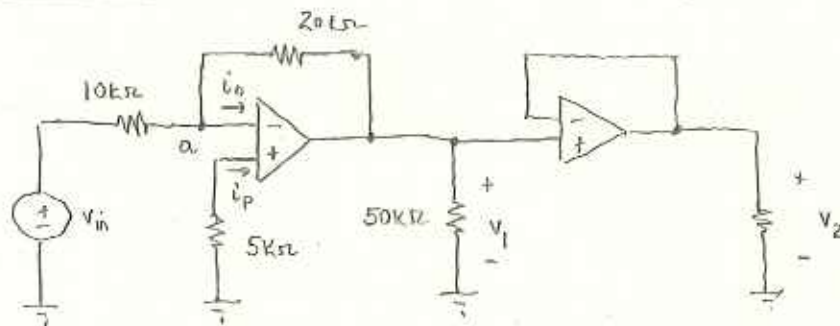
Second interval: $8 \leq t < 12$ secs

$$\text{slope} = \frac{-24 - 24}{4} = -12$$

$$\text{so } i = C \frac{dv}{dt} = 0.25 \times -12 = -3 \text{ A (also constant)}$$



Question 4



(a) In the first op-amp, at node a: $\frac{V_a - V_{in}}{10k} + \frac{V_a - V_1}{20k} + i_{in} = 0$

(x 20k) $2V_a - 2V_{in} + V_a - V_1 = 0$

But $V_a = 0$, so $-2V_{in} - V_1 = 0$
 $V_1 = -2V_{in}$

The closed-loop gain $A_{v1} = \frac{V_1}{V_{in}} = -2$

In the second op-amp V_1 appears on both input terminals of the op-amp. Then, because the inverting input is connected directly to the output,

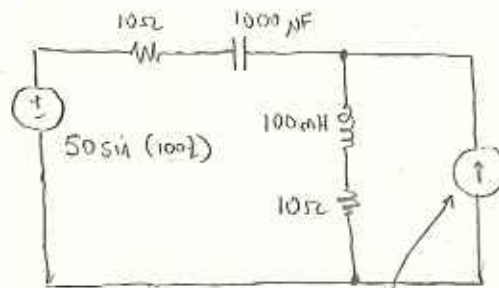
$V_2 = V_1$ so $A_{v2} = \frac{V_2}{V_1} = 1$

(b) Because the op-amps are powered by external voltage sources, the output V_1 and V_2 cannot exceed these voltages

Calculation	V_{in}	V_1	V_2	Explanation
(i)	6.0	-12	0	first op-amp OK, second saturates
(ii)	-7.0	+14	+14	both op-amps OK
(iii)	8.0	-15	0	both op-amps saturate
(iv)	-9.0	+15	+15	first op-amp saturate, second OK

Question 5

(a)



$$\begin{aligned} & 5/\sqrt{2} \cos(100t) \text{ rms Amps} \\ & = \sqrt{2} \times 5/\sqrt{2} \cos(100t) \\ & = 5 \cos(100t) \end{aligned}$$

Impedances: 1000 μF capacitor

$$Z_c = \frac{1}{j\omega C} = \frac{1}{j(100)(1000 \times 10^{-6})}$$

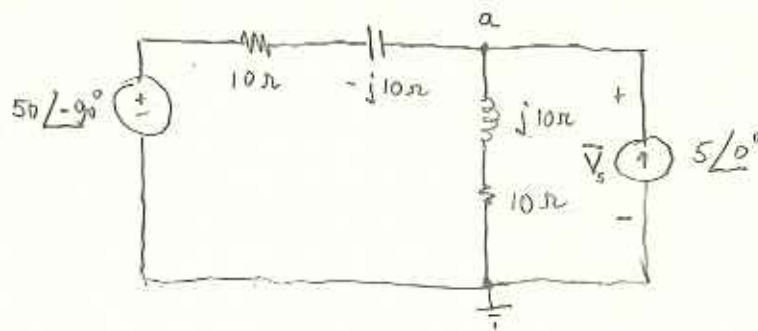
$$= -j10 \Omega$$

100 mH inductor

$$Z_L = j\omega L = j(100)(0.1)$$

$$= j10 \Omega$$

Redrawing the circuit



$$\text{At node } a: \frac{\bar{V}_a - 50 \angle -90^\circ}{10 - j10} + \frac{\bar{V}_a}{10 + j10} - 5 = 0$$

$$[\times (10 - j10)(10 + j10)]$$

$$\begin{aligned} (\bar{V}_a - (-j50))(10 + j10) + \bar{V}_a(10 - j10) &= 5(10 - j10)(10 + j10) \\ (\bar{V}_a + j50)(10 + j10) + \bar{V}_a(10 - j10) &= 5(100 + j100 - j100 + 100) \end{aligned}$$

$$10\bar{V}_a + j10\bar{V}_a + j500 - 500 + 10\bar{V}_a - j10\bar{V}_a = 1000$$

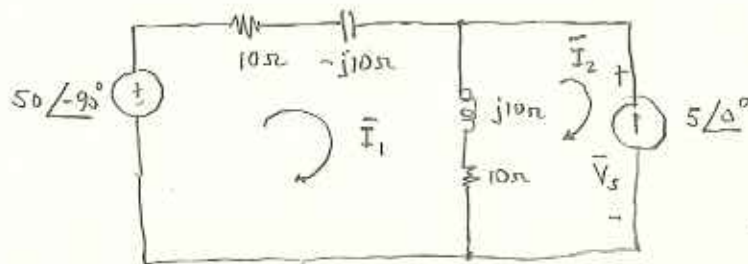
$$20\bar{V}_a - 500 + j500 = 1000$$

$$20 \bar{V}_a = 1500 - j500$$

$$\bar{V}_a = 75 - j25 = 79.0569 \angle -18.435^\circ$$

$$\text{Therefore } v_s(t) = v_a(t) = 79.0569 \cos(100t - 18.435^\circ)$$

Alternatively, using the mesh-current method



$$\text{mesh } \bar{I}_2: \quad \bar{I}_2 = -5 \angle 0^\circ$$

$$\text{Mesh } \bar{I}_1: \quad -50 \angle -90^\circ + (10 - j10) \bar{I}_1 + (10 + j10)(\bar{I}_1 - \bar{I}_2) = 0$$

$$j50 + 10 \bar{I}_1 - j10 \bar{I}_1 + 10 \bar{I}_1 + j10 \bar{I}_1 - 10 \bar{I}_2 - j10 \bar{I}_2 = 0$$

$$j50 + 20 \bar{I}_1 - (10 + j10) \bar{I}_2 = 0$$

$$j50 + 20 \bar{I}_1 - (10 + j10)(-5) = 0$$

$$20 \bar{I}_1 = -50 - j50 - j50$$

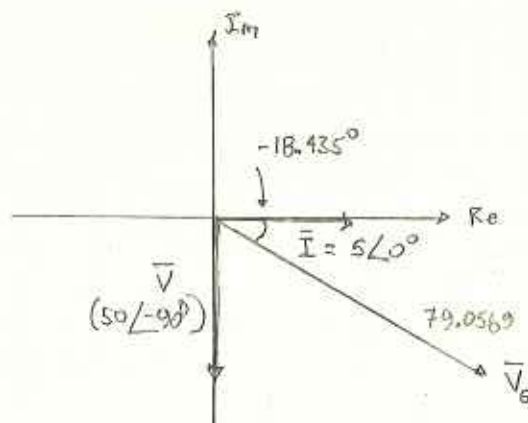
$$\bar{I}_1 = -2.5 - j5$$

$$\text{And } \bar{V}_s = (\bar{I}_1 - \bar{I}_2)(10 + j10) = (-2.5 - j5 + 5)(10 + j10)$$

$$\bar{V}_s = (2.5 - j5)(10 + j10) = 25 - j50 + j25 + 50$$

$$\bar{V}_s = 75 - j25 = 79.0569 \angle -18.435^\circ, \text{ as above}$$

(c) Phasor diagram



Question 6

(a) Output torque: $T_{out} = P_{out} / \omega_m$

$$\text{where } \omega_m = 2\pi n_m / 60 = 2\pi (1500) / 60 \\ = 157.0796 \text{ rad/sec}$$

$$\text{so } T_{out} = \frac{10 \text{ HP} \times 746}{\omega_m} = 47.49 \text{ Nm}$$

Field power loss: $P_F = \frac{V_T^2}{R_F} = \frac{(300)^2}{150} = 600 \text{ W}$

Armature power loss: $P_A = I_A^2 R_A$

$$\text{where } I_A = I_L - I_F = 34.5 - \frac{V_T}{R_F} = 32.5 \text{ A}$$

$$\text{giving } P_A = (32.5)^2 (2.168 \Omega) = 2289.95 \text{ W}$$

Induced voltage: $E_A = V_T - I_A R_A$
 $= 300 - 32.5 \times 2.168 = 229.54 \text{ V}$

Efficiency: $P_{out} = 10 \times 746 = 7460 \text{ W}$
 $P_{in} = V_T I_L = 300 \times 34.5 = 10350 \text{ W}$

$$\eta = \frac{7460}{10350} \times 100\% = 72.077\%$$

(b) We may determine the machine constant from the information given

$$k\phi = \frac{E_A}{\omega_m} = \frac{229.077}{157.0796} = 1.4613$$

The increase in torque causes an increase in I_A

$$I_A = \frac{T_{out}}{k\phi} = \frac{100}{1.4613} = 68.432 \text{ A}$$

Alternatively, we may determine I_A through proportionality

$$\frac{T_1}{T_2} = \frac{I_{A1}}{I_{A2}} \Rightarrow \frac{100}{47.49} = \frac{I_{A1}}{32.5}$$

$$I_{A1} = \frac{32.5}{47.49} \times 100 = 68.432 \text{ A}$$

This changes the induced voltage

$$\begin{aligned} E_A &= V_T - I_A R_A \\ &= 300 - (68.432)(2.160) \\ &= 151.63 \text{ V} \end{aligned}$$

which will change the speed

$$\omega_m = \frac{E_A}{k\phi} = \frac{151.63}{1.4613} = 103.765 \text{ rad/sec}$$

$$\text{so } n_m = 60 \times \frac{\omega_m}{2\pi} = 990.88 \text{ rpm}$$